

**FAILURE DETECTION APPARATUS FOR
AN INTERNAL COMBUSTION ENGINE**

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a failure detection apparatus for an internal combustion engine, and more particularly, to techniques enabling reliable detection of abnormality in an air flow sensor.

10

Description of the Related Art

Recently, in order to prevent harmful exhaust gas from being emitted from an engine mounted on a motor vehicle, various control means are used to improve exhaust gas
15 characteristics. These control means operate based on information supplied from various sensors and the like, to improve the exhaust gas characteristics.

If any of the sensors etc. fails, however, the exhaust gas characteristics may possibly be deteriorated, and
20 accordingly, there has been a demand for reliable detection of failure of such sensors etc. Recently, vehicles equipped with an on-board diagnostic system (OBD etc.) have been developed and put to practical use, with a view to further improving the exhaust gas characteristics.

25 Information from the various sensors etc., especially, information from an air flow sensor (AFS) is used for many purposes including the control of an after-treatment device, EGR or exhaust gas recirculation, etc., and failure of the air flow sensor greatly affects the exhaust gas
30 characteristics. Accordingly, diagnosis of the air flow sensor is of especial importance.

Thus, an apparatus has been proposed in which, when the rotation speed of the engine is lower than or equal to

a predetermined value and at the same time an intake air quantity detected by the air flow sensor is higher than or equal to a predetermined value, for example, the air flow sensor is judged to be abnormal (see Japanese Patent

5 Application Publication No. H10-018897, for example).

In such diagnosis of the air flow sensor, failure of the sensor is usually determined by comparing a reference value set in advance based on operating conditions, such as engine speed, fuel injection quantity, engine torque,
10 throttle opening (throttle valve opening), manifold air pressure, etc., with an output value from the air flow sensor.

However, in the case where the flow rate of exhaust gas is adjusted by an exhaust flow control valve arranged
15 in the intake or exhaust system to promote purification of the exhaust gas or where EGR gas is introduced into the intake system while the exhaust flow rate is adjusted, the quantity of fresh air varies depending on the opening of the exhaust flow control valve or EGR valve, giving rise to
20 a problem that failure of the air flow sensor cannot be determined with accuracy.

To solve the problem, the diagnosis of the air flow sensor may be suspended while the opening of the exhaust flow control valve or EGR valve varies, for example. In
25 the apparatus disclosed in the aforementioned publication, for example, the diagnosis of the air flow sensor as to abnormality is prohibited when the engine is in a cold state in which the engine is supplied with bypass air.

Such suspension of the diagnosis is, however, not
30 desirable because it leads to a substantial reduction in the period for diagnosing the air flow sensor.

SUMMARY OF THE INVENTION

The present invention was created to solve the above problems, and an object thereof is to provide a failure detection apparatus for an internal combustion engine which is capable of reliable detection of abnormality in an air flow sensor irrespective of exhaust flow rate control.

To achieve the object, a failure detection apparatus according to the present invention comprises: fresh air quantity detecting means arranged in an intake system of an internal combustion engine, for detecting a quantity of fresh air introduced into a combustion chamber of the engine; fresh air quantity reference value setting means for setting a reference value for the fresh air quantity in accordance with an operating state of the engine; failure detecting means for detecting abnormality of the fresh air quantity detecting means, based on a result of comparison between the fresh air quantity detected by the fresh air quantity detecting means and the reference value set by the fresh air quantity reference value setting means; exhaust flow rate adjusting means arranged in at least one of the intake system and exhaust system of the engine, for adjusting an exhaust flow rate; target adjustment setting means for setting a target adjustment amount for the exhaust flow rate adjusting means in accordance with the operating state of the engine such that an air-fuel ratio or excess air ratio of the exhaust system becomes equal to a predetermined value corresponding to the operating state; and exhaust flow rate control means for controlling the exhaust flow rate adjusting means in accordance with the target adjustment amount set by the target adjustment setting means, wherein the fresh air quantity reference value setting means sets the reference value in accordance with not only the operating state of the engine but also the target adjustment amount set for the exhaust flow rate

adjusting means by the target adjustment setting means.

Thus, the reference value for the fresh air quantity is set by the fresh air quantity reference value setting means in accordance with the operating state (engine speed, fuel injection quantity, engine torque, throttle opening, manifold air pressure, etc.) of the engine, and based on the result of comparison between the thus-set reference value and the fresh air quantity detected by the fresh air quantity detecting means, abnormality or failure of the fresh air quantity detecting means (air flow sensor) is detected. In this case, the fresh air quantity reference value setting means sets the reference value in accordance with not only the operating state of the engine but also the target adjustment amount set for the exhaust flow rate adjusting means by the target adjustment setting means.

Accordingly, the reference value for the fresh air quantity can be set taking account of the target adjustment amount, that is, the amount of exhaust flow rate adjusted by the exhaust flow rate adjusting means. Proper and reliable diagnosis of the fresh air quantity detecting means can therefore be carried out, irrespective of the adjustment of exhaust flow rate for promoting exhaust gas purification, whereby reliability of the fresh air quantity detecting means can be enhanced, making it possible to further improve the exhaust gas characteristics.

In the failure detection apparatus according to the present invention, the exhaust flow rate adjusting means may include at least one of an intake throttle valve arranged in the intake system for adjusting the fresh air quantity and an exhaust throttle valve arranged in the exhaust system for directly adjusting the exhaust flow rate. The fresh air quantity reference value setting means sets the reference value in accordance with not only the

operating state of the engine but also a target valve opening set for said at least one of the intake and exhaust throttle valves by the target adjustment setting means.

Thus, the fresh air quantity reference value setting
5 means sets the reference value in accordance with not only the operating state of the engine but also the target valve opening set for the intake and exhaust throttle valves by the target adjustment setting means.

Accordingly, the reference value for the fresh air
10 quantity can be set taking account of the target valve opening, that is, the amount of exhaust flow rate adjusted by the intake and exhaust throttle valves. Proper and reliable diagnosis of the fresh air quantity detecting means can therefore be carried out, irrespective of the
15 adjustment of exhaust flow rate for promoting exhaust gas purification, whereby reliability of the fresh air quantity detecting means can be enhanced.

The failure detection apparatus of the present invention may further comprise exhaust concentration
20 detecting means for detecting an exhaust concentration to thereby detect the air-fuel ratio or excess air ratio of the exhaust system, wherein the fresh air quantity reference value setting means corrects the target adjustment amount for the exhaust flow rate adjusting means,
25 based on a difference between the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, and the predetermined value, and sets the reference value based on the corrected target adjustment amount.

30 Specifically, the target adjustment amount for the exhaust flow rate adjusting means is a command value which is set in accordance with the operating state (engine speed, fuel injection quantity, etc.) of the engine such that the

air-fuel ratio or excess air ratio of the exhaust system becomes equal to the predetermined value corresponding to the operating state, and the target adjustment amount may possibly be different from an actual adjustment amount.

5 Accordingly, the target adjustment amount for the exhaust flow rate adjusting means is corrected based on the difference between the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, and the predetermined value,
10 and the reference value is set based on the corrected target adjustment amount.

Consequently, the reference value for the fresh air quantity can be set to a proper value matching the actual adjustment amount for the exhaust flow rate adjusting means,
15 and the fresh air quantity detecting means can be diagnosed with higher accuracy during the adjustment of the exhaust flow rate, whereby the reliability of the fresh air quantity detecting means can be further improved.

The failure detection apparatus of the present
20 invention may further comprise exhaust concentration detecting means for detecting an exhaust concentration to thereby detect the air-fuel ratio or excess air ratio of the exhaust system, wherein the exhaust flow rate control means corrects an amount of adjustment by the exhaust flow
25 rate adjusting means such that the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, coincides with the predetermined value.

As mentioned above, the target adjustment amount for
30 the exhaust flow rate adjusting means may possibly be different from an actual adjustment amount, and therefore, the amount of adjustment by the exhaust flow rate adjusting means is corrected such that the air-fuel ratio or excess

air ratio of the exhaust system, detected by the exhaust concentration detecting means, coincides with the predetermined value.

Accordingly, the reference value for the fresh air
5 quantity can be set to a proper value matching the actual amount of adjustment by the exhaust flow rate adjusting means, whereby the fresh air quantity detecting means can be diagnosed with higher accuracy during the adjustment of the exhaust flow rate, making it possible to further
10 improve the reliability of the fresh air quantity detecting means.

The failure detection apparatus of the present invention may further comprise exhaust concentration detecting means for detecting an exhaust concentration to
15 thereby detect the air-fuel ratio or excess air ratio of the exhaust system, wherein, when the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, is different from the predetermined value, the fresh air quantity reference
20 value setting means suspends the control of the exhaust flow rate adjusting means by the exhaust flow rate control means and sets the reference value based solely on the operating state of the engine.

The target adjustment amount for the exhaust flow rate
25 adjusting means may possibly be different from an actual adjustment amount, as mentioned above, and therefore, when the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, is different from the predetermined value, the
30 control of the exhaust flow rate adjusting means is suspended.

In this case, the reference value for the fresh air quantity is set based solely on the operating state of the

engine, to enhance the accuracy of diagnosis of the fresh air quantity detecting means without reducing the occasion for diagnosis, whereby the reliability of the fresh air quantity detecting means can be further improved.

5 According to another aspect of the present invention, a failure detection apparatus comprises: fresh air quantity detecting means arranged in an intake system of an internal combustion engine, for detecting a quantity of fresh air introduced into a combustion chamber of the engine; fresh
10 air quantity reference value setting means for setting a reference value for the fresh air quantity in accordance with an operating state of the engine; failure detecting means for detecting abnormality of the fresh air quantity detecting means, based on a result of comparison between
15 the fresh air quantity detected by the fresh air quantity detecting means and the reference value set by the fresh air quantity reference value setting means; exhaust flow rate adjusting means arranged in one of the intake system and exhaust system of the engine, for adjusting an exhaust
20 flow rate; target adjustment setting means for setting a target adjustment amount for the exhaust flow rate adjusting means in accordance with the operating state of the engine such that an air-fuel ratio or excess air ratio of the exhaust system becomes equal to a predetermined
25 value corresponding to the operating state; exhaust flow rate control means for controlling the exhaust flow rate adjusting means in accordance with the target adjustment amount set by the target adjustment setting means; an EGR passage for allowing part of exhaust gas to be recirculated
30 from the exhaust system of the engine to the intake system as EGR gas; an EGR valve inserted in the EGR passage, for controlling a quantity of the EGR gas by varying an opening thereof; target opening setting means for setting a target

EGR valve opening for the EGR valve in accordance with the operating state of the engine such that the air-fuel ratio or excess air ratio of the exhaust system becomes equal to the predetermined value; and EGR valve control means for
5 controlling the EGR valve in accordance with the target EGR valve opening set by the target opening setting means, wherein the fresh air quantity reference value setting means sets the reference value in accordance with not only the operating state of the engine but also the target
10 adjustment amount set for the exhaust flow rate adjusting means by the target adjustment setting means and the target EGR valve opening set by the target opening setting means.

Thus, the reference value for the fresh air quantity is set by the fresh air quantity reference value setting
15 means in accordance with the operating state (engine speed, fuel injection quantity, engine torque, throttle opening, manifold air pressure, etc.) of the engine, and based on the result of comparison between the thus-set reference value and the fresh air quantity detected by the fresh air
20 quantity detecting means, abnormality or failure of the fresh air quantity detecting means (air flow sensor) is detected. In this case, the fresh air quantity reference value setting means sets the reference value in accordance with not only the operating state of the engine but also
25 the target adjustment amount set for the exhaust flow rate adjusting means by the target adjustment setting means and the target EGR valve opening set by the target opening setting means.

Accordingly, the reference value for the fresh air
30 quantity can be set taking account of the target adjustment amount, that is, the amount of exhaust flow rate adjusted by the exhaust flow rate adjusting means, and the target EGR valve opening, that is, the EGR gas quantity. Proper

and reliable diagnosis of the fresh air quantity detecting means can therefore be carried out, irrespective of the adjustment of exhaust flow rate or the introduction of EGR gas for promoting exhaust gas purification, whereby

5 reliability of the fresh air quantity detecting means can be enhanced, making it possible to further improve the exhaust gas characteristics.

In the failure detection apparatus of the present invention, the exhaust flow rate adjusting means may
10 include at least one of an intake throttle valve arranged in the intake system for adjusting the fresh air quantity and an exhaust throttle valve arranged in the exhaust system for directly adjusting the exhaust flow rate. The fresh air quantity reference value setting means sets the
15 reference value in accordance with not only the operating state of the engine but also a target valve opening set for said at least one of the intake and exhaust throttle valves by the target adjustment setting means and the target EGR valve opening set by the target opening setting means.

20 Thus, the fresh air quantity reference value setting means sets the reference value in accordance with not only the operating state of the engine but also the target valve opening set for the intake and exhaust throttle valves by the target adjustment setting means and the target EGR
25 valve opening set by the target opening setting means.

Accordingly, the reference value for the fresh air quantity can be set taking account of the target valve opening, that is, the amount of exhaust flow rate adjusted by the intake and exhaust throttle valves, as well as the
30 target EGR valve opening, that is, the EGR gas quantity. Proper and reliable diagnosis of the fresh air quantity detecting means can therefore be carried out, irrespective of the adjustment of exhaust flow rate or the introduction

of EGR gas for promoting exhaust gas purification, whereby reliability of the fresh air quantity detecting means can be enhanced.

The failure detection apparatus of the present invention may further comprise exhaust concentration detecting means for detecting an exhaust concentration to thereby detect the air-fuel ratio or excess air ratio of the exhaust system, wherein the fresh air quantity reference value setting means corrects at least one of the target adjustment amount and the target EGR valve opening based on a difference between the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, and the predetermined value, and sets the reference value based on said at least one of the corrected target adjustment amount and the corrected target EGR valve opening.

Specifically, the target adjustment amount for the exhaust flow rate adjusting means or the target EGR valve opening for the EGR valve is a command value which is set in accordance with the operating state (engine speed, fuel injection quantity, etc.) of the engine such that the air-fuel ratio or excess air ratio of the exhaust system becomes equal to the predetermined value corresponding to the operating state, and may possibly be different from an actual adjustment amount or actual EGR valve opening. Thus, the target adjustment amount for the exhaust flow rate adjusting means and the target EGR valve opening are corrected based on the difference between the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, and the predetermined value, and the reference value is set based on the corrected target adjustment amount and the corrected target EGR valve opening.

Accordingly, the reference value for the fresh air quantity can be set to a proper value matching the actual adjustment amount of the exhaust flow rate adjusting means and the actual EGR valve opening, and thus the fresh air quantity detecting means can be diagnosed with higher accuracy, further improving the reliability of the fresh air quantity detecting means.

The failure detection apparatus of the present invention may further comprise exhaust concentration detecting means for detecting an exhaust concentration to thereby detect the air-fuel ratio or excess air ratio of the exhaust system, wherein the exhaust flow rate control means corrects an amount of adjustment by the exhaust flow rate adjusting means such that the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, coincides with the predetermined value, and the EGR valve control means corrects the opening of the EGR valve such that the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, coincides with the predetermined value.

As mentioned above, the target adjustment amount for the exhaust flow rate adjusting means and the target EGR valve opening for the EGR valve may possibly be different from actual adjustment amount and EGR valve opening, respectively. Thus, the amount of adjustment by the exhaust flow rate adjusting means and the EGR valve opening are corrected such that the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, coincides with the predetermined value.

Accordingly, the reference value for the fresh air quantity can be set to a proper value matching the actual

amount of adjustment by the exhaust flow rate adjusting means and the actual EGR valve opening, and thus the fresh air quantity detecting means can be diagnosed with higher accuracy, further improving the reliability of the fresh
5 air quantity detecting means.

The failure detection apparatus of the present invention may further comprise exhaust concentration detecting means for detecting an exhaust concentration to thereby detect the air-fuel ratio or excess air ratio of
10 the exhaust system, wherein, when the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, is different from the predetermined value, the fresh air quantity reference value setting means suspends the control of the exhaust
15 flow rate adjusting means by the exhaust flow rate control means as well as the control of the EGR valve by the EGR valve control means and sets the reference value based solely on the operating state of the engine.

The target adjustment amount for the exhaust flow rate
20 adjusting means and the target EGR valve opening for the EGR valve may possibly be different from actual adjustment amount and EGR valve opening, respectively. Thus, when the air-fuel ratio or excess air ratio of the exhaust system, detected by the exhaust concentration detecting means, is
25 different from the predetermined value, the control of the exhaust flow rate adjusting means and the control of the EGR valve are suspended.

In this case, the reference value for the fresh air quantity is set based solely on the operating state of the
30 engine, to enhance the accuracy of diagnosis of the fresh air quantity detecting means without reducing the occasion for diagnosis, whereby the reliability of the fresh air quantity detecting means can be further improved.

A further scope of applicability of the present invention will become apparent from the detailed description given hereinafter. However, it should be understood that the detailed description and specific
5 example, while indicating preferred embodiments of the invention, are given by way of illustration only, since various changes and modifications within the spirit and scope of the invention will become apparent to those skilled in the art from this detailed description.

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BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will become more fully understood from the detailed description given hereinbelow and the accompanying drawings which are given by way of
15 illustration only, and thus, are not limitative of the present invention, and wherein:

FIG. 1 is a diagram illustrating a schematic arrangement of a failure detection apparatus for an internal combustion engine according to the present
20 invention;

FIG. 2 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination according to a first embodiment of the present invention;

FIG. 3 is a flowchart illustrating another control
25 routine for AFS failure determination according to a second embodiment of the present invention;

FIG. 4 is a flowchart illustrating still another control routine for AFS failure determination according to a third embodiment of the present invention;

30 FIG. 5 is a flowchart illustrating yet another control routine for AFS failure determination according to a fourth embodiment of the present invention;

FIG. 6 is a flowchart illustrating a further control

routine for AFS failure determination according to a fifth embodiment of the present invention; and

FIG. 7 is a flowchart illustrating a still further control routine for AFS failure determination according to a sixth embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Embodiments of the present invention will be hereinafter described with reference to the accompanying drawings.

FIG. 1 illustrates a schematic arrangement of a failure detection apparatus for an internal combustion engine according to the present invention. The arrangement of the failure detection apparatus of the present invention will be described first with reference to FIG. 1.

As shown in FIG. 1, an internal combustion engine 1 is a common-rail in-line four-cylinder diesel engine, for example. In the common-rail engine 1, a solenoid-operated fuel injection nozzle 4 is provided for each cylinder so as to face a corresponding combustion chamber 2 and is connected through a high-pressure pipe 5 to a common rail 6. The common rail 6 is connected through a high-pressure pipe 7a to a high-pressure pump 8, which is connected to a fuel tank 9 through a low-pressure pipe 7b. Since the engine 1 is a diesel engine, light oil is used as fuel.

A solenoid-operated intake throttle valve (exhaust flow rate adjusting means) 12 is arranged in an intake passage 10 of the engine 1. On an upstream side of the intake throttle valve 12 is provided an air flow sensor (AFS; fresh air quantity detecting means) 14 for outputting a signal S_{afs} based on which a fresh air quantity Q_a is detected. The intake throttle valve 12 comprises a butterfly valve, for example. Also, in the illustrated

engine, a Karman vortex air flow sensor is used as the air flow sensor 14 by way of example, but a hot-wire air flow sensor or the like may be used instead.

5 An after-treatment device 24 is inserted in an exhaust passage 20. The after-treatment device 24 comprises, for example, a continuously regenerating DPF (diesel particulate filter) including a DPF 24b and an oxidation catalyst 24a arranged on an upstream side of the DPF 24b.

10 In the continuously regenerating DPF, an oxidizer (NO_2) is produced in the oxidation catalyst 24a and is used to continuously remove particulate matter (PM) deposited on the downstream-side DPF 24b by oxidation under a relatively high exhaust gas temperature condition, to thereby regenerate the DPF 24b.

15 A λ sensor (O_2 sensor etc.; exhaust concentration detecting means) 26 is arranged at the exhaust passage 20 at a location upstream the after-treatment device 24, to detect an excess air ratio λ of the exhaust system through detection of the oxygen concentration of exhaust gas.

20 Instead of detecting the excess air ratio λ , the air-fuel ratio may be detected, and in this case, an air-fuel ratio sensor (LAFS etc.) is used in place of the λ sensor 26.

The exhaust passage 20 is also provided with a solenoid-operated exhaust throttle valve (exhaust flow rate

25 adjusting means) 22. The exhaust throttle valve 22 comprises a butterfly valve, for example, like the intake throttle valve 12, and is operated singly or together with the intake throttle valve 12 to adjust the exhaust flow rate, that is, the exhaust flow velocity, and thereby

30 control the temperature of the exhaust gas in the exhaust passage 20 so that purification of the exhaust gas can be promoted at the cold-start of the engine 1, for example. The exhaust throttle valve 22 also functions as an exhaust

brake.

An EGR passage 30 extends from a portion of the exhaust passage 20 near the engine 1, to allow part of the exhaust gas to be recirculated to the intake system as EGR gas. The EGR passage 30 is connected at the other end to a portion of the intake passage 10 located downstream the intake throttle valve 12. A solenoid-operated EGR valve 32 of which the opening can be adjusted to a desired opening is inserted in the EGR passage 30.

10 An electronic control unit (ECU) 40 is connected at an input side thereof with various sensors which include an accelerator position sensor (APS) 44 for detecting the stroke of an accelerator pedal 42, that is, accelerator position θ_{acc} , and a crank angle sensor 46 for detecting an engine speed N_e through detection of crank angle, besides
15 the air flow sensor 14 and the λ sensor 26.

The output side of the ECU 40 is connected with various devices including a failure lamp 50 for indicating a variety of failure statuses, in addition to the fuel
20 injection nozzles 4, intake and exhaust throttle valves 12 and 22, and EGR valve 32.

Based on information input from the various sensors, operations of the various devices are controlled to properly control the operation of the engine 1. For
25 example, based on the information from the accelerator position sensor 44, air flow sensor 14 and λ sensor 26, a fuel injection quantity Q_f as well as the opening of the intake throttle valve 12 are adjusted to control the operation of the engine 1, whereby not only the control of
30 normal engine operation but the regeneration control of the after-treatment device 24, the opening control (exhaust flow rate control means) of the intake and exhaust throttle valves 12 and 22 for promoting exhaust gas purification,

and the opening control (EGR valve control means) of the EGR valve 32 are carried out.

Operation of the failure detection apparatus for the engine configured as above will be now described.

5 A first embodiment will be explained first.

FIG. 2 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed in the failure detection apparatus according to the first embodiment of the present invention. The control routine
10 will be described with reference to the flowchart.

First, in Step S10, it is determined whether or not exhaust flow rate control is under execution, that is, whether or not the exhaust flow rate is being adjusted by controlling the opening of one or both of the intake and
15 exhaust throttle valves 12 and 22 toward the closed position. For example, just after the cold-start of the engine 1, the exhaust gas purifying capability is low, and it is determined in this step whether or not the exhaust flow rate control is executed in such situations to promote
20 exhaust gas purification. If the decision in this step is affirmative (Yes) and thus the exhaust flow rate control is under execution, the routine proceeds to Step S12.

In Step S12 is set a target throttle valve opening for the intake and exhaust throttle valves 12 and 22 as a whole.
25 In this instance, the target throttle valve opening (target adjustment amount, target valve opening) is set (target adjustment setting means) in accordance with the temperature (cooling water temperature etc.) of the engine 1, for example. Usually, a target value (predetermined
30 value) λ_1 for the excess air ratio λ is set in accordance with the operating state of the engine 1, and as the openings of the intake and exhaust throttle valves 12 and 22 change, the exhaust gas or EGR gas is recirculated into

the combustion chamber 2 due to increase in the exhaust pressure, with the result that the excess air ratio λ varies depending on the EGR quantity. Accordingly, the fuel injection quantity Q_f also is controlled in accordance
5 with the target throttle valve opening so that the excess air ratio λ may be kept at the target value λ_1 . In other words, the target throttle valve opening is set while controlling the excess air ratio λ to the target value λ_1 . In practice, a map showing the relationship of the target
10 throttle valve opening with the engine speed N_e , fuel injection quantity Q_f and target value λ_1 is prepared beforehand by experiment, and as soon as the target throttle valve opening is set, an appropriate fuel injection quantity Q_f is read from the map.

15 In Step S14, the target throttle valve opening set in the aforementioned manner is corrected based on an actual excess air ratio λ detected by the λ sensor 26. The target throttle valve opening is merely a command value from the ECU 40 and is not an actual value. Thus, even if the
20 overall opening of the intake and exhaust throttle valves 12 and 22 is controlled so as to coincide with the target throttle valve opening corresponding to the target value λ_1 , a difference can occasionally arise between the actual overall opening of the intake and exhaust throttle valves
25 12 and 22 and the target throttle valve opening. Such an opening difference leads to an increased or decreased air quantity, causing a similar difference between the target value λ_1 and the actual excess air ratio λ . Accordingly, the target value λ_1 is compared with the actual excess air
30 ratio λ , and based on the result of comparison, the target throttle valve opening is corrected so as to match the actual opening.

Specifically, a difference (absolute value) $|\lambda - \lambda_1|$

between the target value λ_1 and the actual excess air ratio λ detected by the λ sensor 26 is obtained, and the target throttle valve opening is corrected by an amount corresponding to the difference. The corrected target
5 throttle valve opening obtained in this manner may be stored as a learned value.

Consequently, the target throttle valve opening is corrected to a proper value matching the actual overall opening of the intake and exhaust throttle valves 12 and 22.

10 In Step S16, a reference value for the fresh air quantity Q_a , that is, a fresh air quantity reference value, is set (fresh air quantity reference value setting means) in accordance with the appropriately corrected target throttle valve opening obtained as described above.

15 Basically, the reference value for the fresh air quantity Q_a , or the fresh air quantity reference value, is set in accordance with the operating state (engine speed N_e , fuel injection quantity Q_f , engine torque, throttle valve opening (throttle opening), manifold air pressure, etc.) of
20 the engine 1. In this step, the fresh air quantity reference value thus set is corrected by using the target throttle valve opening. In practice, a map showing the relationship between fresh air quantity Q_a' applicable during the exhaust flow rate control and the target
25 throttle valve opening is prepared beforehand, and an appropriate fresh air quantity Q_a' read from the map is set as the fresh air quantity reference value.

Since the target throttle valve opening has been corrected to a proper value matching the actual overall
30 opening of the intake and exhaust throttle valves 12 and 22, as mentioned above, the fresh air quantity reference value can be set to a highly accurate value as in the case where the exhaust flow rate is not controlled through the

adjustment of the intake and exhaust throttle valves 12 and 22.

If the decision in Step S10 is negative (No) and it is judged that the exhaust flow rate control is not under
5 execution, the routine proceeds to Step S20.

In this case, a fresh air quantity Q_a normally obtained in accordance with the operating state of the engine 1 is set directly as the fresh air quantity reference value, without regard to the target throttle
10 valve opening.

In Step S22, a difference (absolute value) $|S_{afs} - \text{reference value}|$ between the output signal S_{afs} of the air flow sensor 14 and the fresh air quantity reference value is derived as X ($|S_{afs} - \text{reference value}| = X$). Namely, if
15 the air flow sensor 14 is functioning normally, its output signal S_{afs} should coincide with the fresh air quantity reference value. In the event the output signal S_{afs} differs from the fresh air quantity reference value, the difference is derived as X in this step.

20 Then, in Step S24, it is determined whether or not the difference X has a value larger than or equal to a predetermined value X_1 (very small value) ($X \geq X_1$).

If the decision in Step S24 is affirmative (Yes) and it is judged that the difference X is larger than or equal
25 to the predetermined value X_1 , it can be concluded that the air flow sensor 14 is not functioning normally and is in an abnormal state and that failure of the air flow sensor 14 has occurred (failure detecting means). In this case, therefore, it is ascertained in Step S26 that the
30 difference X remains larger than or equal to the predetermined value X_1 for a predetermined time t_1 , and in Step S28, the failure lamp 50 is turned on to notify the driver of the failure of the air flow sensor 14. Also, in

Step S30, a failure code corresponding to the failure of the air flow sensor 14 is recorded in a memory within the ECU 40.

Since the fresh air quantity reference value, in particular, is set with high accuracy based on the proper target throttle valve opening just as in the case where the intake and exhaust throttle valves 12 and 22 are not operated, failure of the air flow sensor 14 can be detected with precision, regardless of the adjustment of the exhaust flow rate, and the reliability of the air flow sensor 14 can be improved. Thus, in cases where the output information from the air flow sensor 14 is used for controlling the regeneration of the after-treatment device 24, the regeneration can be controlled optimally, making it possible to further improve the exhaust gas characteristics.

If the decision in Step S24 is negative (No) and it is judged that the difference X is smaller than the predetermined value X_1 (very small value), it can be concluded that the air flow sensor 14 is functioning normally without failure, and thus the subsequent steps of the routine are not executed.

A second embodiment will be now described.

FIG. 3 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed in the failure detection apparatus according to the second embodiment of the present invention. In the following description of the flowchart, only the differences between the first and second embodiments will be explained.

In the second embodiment, after the target throttle valve opening is set in Step S12, the fresh air quantity reference value is set immediately thereafter based on the target throttle valve opening in Step S16, without correcting the target throttle valve opening, unlike the

first embodiment.

Then, in Step S17, it is determined whether or not the actual excess air ratio λ detected by the λ sensor 26 is equal to the target value λ_1 ($\lambda = \lambda_1$). In other words, it is determined whether or not a difference between the target value λ_1 and the actual excess air ratio λ has been caused due to an opening difference between the actual overall opening of the intake and exhaust throttle valves 12 and 22 and the target throttle valve opening.

10 If the decision in Step S17 is affirmative (Yes) and it is judged that the actual excess air ratio λ and the target value λ_1 are equal to each other, it can be concluded that the target throttle valve opening has been set to a proper value matching the actual overall opening of the intake and exhaust throttle valves 12 and 22, and accordingly, the routine proceeds to Step S22.

On the other hand, if the decision in Step S17 is negative (No) and it is judged that the actual excess air ratio λ and the target value λ_1 differ from each other, the overall opening of the intake and exhaust throttle valves 12 and 22 is corrected, in Step S18, such that the actual excess air ratio λ becomes equal to the target value λ_1 .

Namely, in the first embodiment, the target throttle valve opening is corrected so as to match the actual overall opening of the intake and exhaust throttle valves 12 and 22. In the second embodiment, the actual overall opening of the intake and exhaust throttle valves 12 and 22 is corrected so as to match the target throttle valve opening.

30 Thus, the actual overall opening of the intake and exhaust throttle valves 12 and 22 is corrected to a proper value matching the target throttle valve opening, and accordingly, the fresh air quantity reference value can be

set to a highly accurate value as in the case where the intake and exhaust throttle valves 12 and 22 are not operated.

Consequently, failure of the air flow sensor 14 can be
5 detected with precision, regardless of the adjustment of the exhaust flow rate, and the reliability of the air flow sensor 14 can be improved. In cases where the information from the air flow sensor 14 is used for controlling the regeneration of the after-treatment device 24, therefore,
10 the regeneration can be controlled optimally, making it possible to further improve the exhaust gas characteristics.

A third embodiment will be now described.

FIG. 4 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed
15 in the failure detection apparatus according to the third embodiment of the present invention. In the following description of the flowchart, only the differences between the third embodiment and the first or second embodiment will be explained.

20 In the third embodiment, after the target throttle valve opening is set in Step S12, the fresh air quantity reference value is set immediately thereafter based on the target throttle valve opening in Step S16, like the second embodiment.

25 Then, in Step S17, it is determined whether or not the actual excess air ratio λ detected by the λ sensor 26 is equal to the target value λ_1 ($\lambda = \lambda_1$), as in the second embodiment.

If the decision in Step S17 is affirmative (Yes) and
30 it is judged that the actual excess air ratio λ and the target value λ_1 are equal to each other, it can be concluded that the target throttle valve opening has been set to a proper value matching the actual overall opening

of the intake and exhaust throttle valves 12 and 22, and accordingly, the routine proceeds to Step S22.

On the other hand, if the decision in Step S17 is negative (No) and it is judged that the actual excess air ratio λ and the target value λ_1 differ from each other, the exhaust flow rate control is suspended in Step S19, then a normally obtained fresh air quantity Q_a is directly set as the fresh air quantity reference value in Step S20, and the routine proceeds to Step S22.

Namely, in the third embodiment, if there is a difference between the actual excess air ratio λ and the target value λ_1 , it is concluded that the fresh air quantity reference value cannot be set with accuracy, and the exhaust flow rate control itself is suspended. Thus, using the fresh air quantity Q_a obtained normally in accordance with the operating state of the engine 1 as the fresh air quantity reference value, the air flow sensor 14 is diagnosed, without adjusting the exhaust flow rate.

In this case, the diagnosis of the air flow sensor 14 is not suspended but is continuously performed even while the exhaust flow rate control is suspended, whereby the occasion for diagnosis is not reduced.

Consequently, the fresh air quantity reference value can always be set to an accurate value, regardless of the degree to which the exhaust flow rate is adjusted. Thus, failure of the air flow sensor 14 can be detected with precision, making it possible to improve the reliability of the air flow sensor 14.

Fourth to sixth embodiments will be now described.

In the fourth to sixth embodiments, failure of the air flow sensor is determined taking account of not only the exhaust flow rate control, as in the first to third embodiments described above, but also EGR control. The

fourth to sixth embodiments correspond to the first to third embodiments, respectively.

FIG. 5 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed
5 in the failure detection apparatus according to the fourth embodiment of the present invention. In the following description of the flowchart, only the differences between the fourth and first embodiments will be explained.

First, in Step S10, it is determined whether or not
10 the exhaust flow rate control is under execution, that is, whether or not the exhaust flow rate is being adjusted by controlling the opening of one or both of the intake and exhaust throttle valves 12 and 22 toward the closed position, as in the foregoing embodiments. If the decision
15 in this step is affirmative (Yes) and thus the exhaust flow rate control is under execution, the routine proceeds to Step S11.

In Step S11, it is determined whether or not the EGR is under execution, that is, whether or not the EGR valve
20 32 is opened to introduce the EGR gas into the intake system while the exhaust flow rate control is performed. If the decision in this step is affirmative (Yes) and thus the EGR is under execution, the routine proceeds to Step S12'.

25 In Step S12' are set a target throttle valve opening for the intake and exhaust throttle valves 12 and 22 as a whole and a target EGR valve opening for the EGR valve 32. In this instance, the target throttle valve opening (target adjustment amount) is set (target adjustment setting means)
30 in accordance with the temperature (cooling water temperature etc.) of the engine 1, as mentioned above, and the target EGR valve opening is set (target opening setting means) in accordance with the engine speed N_e and the fuel

injection quantity Q_f .

Usually, the target value (predetermined value) λ_1 for the excess air ratio λ is set in accordance with the operating state of the engine 1, and as the openings of the intake and exhaust throttle valves 12 and 22 change, the exhaust gas or EGR gas is recirculated into the combustion chamber 2, as mentioned above, with the result that the excess air ratio λ varies depending on the EGR quantity. Accordingly, the fuel injection quantity Q_f also is controlled in accordance with the target throttle valve opening so that the excess air ratio λ may be kept at the target value λ_1 . In other words, the target throttle valve opening is set while controlling the excess air ratio λ to the target value λ_1 . In practice, the fuel injection quantity Q_f is read from the map prepared beforehand, as mentioned above.

Also, as the target value λ_1 changes, the quantity of the EGR gas introduced, that is, the target EGR valve opening, also changes with relation to the opening of the intake throttle valve 12 and the fuel injection quantity Q_f . Accordingly, the target EGR valve opening is set also based on the target value λ_1 for the excess air ratio λ . In practice, a map showing the relationship of the target EGR valve opening with the engine speed N_e , fuel injection quantity Q_f and target value λ_1 is prepared beforehand by experiment, and an appropriate target EGR valve opening is read from the map.

In Step S14', the target throttle valve opening and target EGR valve opening set in the aforementioned manner are corrected based on an actual excess air ratio λ detected by the λ sensor 26. The target throttle valve opening and the target EGR valve opening are merely command values from the ECU 40 and are not actual values. Thus,

even if the overall opening of the intake and exhaust throttle valves 12 and 22 is controlled so as to coincide with the target throttle valve opening corresponding to the target value λ_1 and also the opening of the EGR valve 32 is controlled so as to coincide with the target EGR valve opening corresponding to the target value λ_1 , a difference can occasionally arise between the actual overall opening of the intake and exhaust throttle valves 12 and 22 and the target throttle valve opening or between the actual opening of the EGR valve 32 and the target EGR valve opening. Such an opening difference causes a similar difference between the target value λ_1 and the actual excess air ratio λ . Accordingly, the target value λ_1 is compared with the actual excess air ratio λ , and based on the result of comparison, the target throttle valve opening and the target EGR valve opening are corrected so as to match their actual openings.

Specifically, a difference (absolute value) $|\lambda - \lambda_1|$ between the target value λ_1 and the actual excess air ratio λ detected by the λ sensor 26 is obtained, and the target throttle valve opening and the target EGR valve opening are corrected by an amount corresponding to the difference. In this case, the target throttle valve opening and the target EGR valve opening may be corrected as a whole based on the difference $|\lambda - \lambda_1|$.

In Step S16', a reference value for the fresh air quantity Q_a , that is, the fresh air quantity reference value, is set (fresh air quantity reference value setting means) in accordance with the target throttle valve opening and target EGR valve opening obtained as described above. Basically, the reference value for the fresh air quantity Q_a , or the fresh air quantity reference value, is set in accordance with the operating state (engine speed N_e , fuel

injection quantity Q_f , engine torque, throttle opening, manifold air pressure, etc.) of the engine 1. In this step, the fresh air quantity reference value thus set is corrected by using the target throttle valve opening and the target EGR valve opening. In practice, a map showing the relationship between fresh air quantity Q_a' applicable during the exhaust flow rate control and the target throttle valve opening is prepared beforehand, a difference ($Q_a' - Q_{egr}$) between the fresh air quantity Q_a' read from the map and an EGR gas quantity Q_{egr} corresponding to the target EGR valve opening is obtained, and a reference value corresponding to the difference ($Q_a' - Q_{egr}$) is set as the fresh air quantity reference value. Alternatively, the reference value for the fresh air quantity Q_a' not including the EGR gas may be corrected by using a value corresponding to the target EGR valve opening.

Since the target throttle valve opening and the target EGR valve opening have been corrected as a whole to proper values matching the actual openings of the intake and exhaust throttle valves 12 and 22 and EGR valve 32, as mentioned above, the fresh air quantity reference value can be set to a highly accurate value as in the case where the exhaust flow rate is not adjusted or the EGR gas is not introduced.

If the decision in Step S10 is negative (No) and it is judged that the exhaust flow rate control is not under execution, or if the decision in Step S11 is negative (No) and it is judged that no EGR gas is being introduced into the intake system, the routine proceeds to Step S20.

In this case, a fresh air quantity Q_a normally obtained in accordance with the operating state of the engine 1 is set directly as the fresh air quantity reference value, without regard to the target throttle

valve opening or the target EGR valve opening.

Then, in Step S22, a difference (absolute value) $|S_{afs} - \text{reference value}|$ between the output signal S_{afs} of the air flow sensor 14 and the fresh air quantity reference value is derived as X ($|S_{afs} - \text{reference value}| = X$), like the foregoing embodiments. Subsequently, in Step S24, it is determined whether or not the difference X has a value larger than or equal to the predetermined value X_1 (very small value) ($X \geq X_1$). If the decision in this step is affirmative (Yes) and it is judged that the difference X is larger than or equal to the predetermined value X_1 , it is concluded that failure of the air flow sensor 14 has occurred (failure detecting means), and the failure lamp 50 is turned on, in Step S28, to notify the driver of the failure of the air flow sensor 14. Also, in Step S30, the failure code corresponding to the failure of the air flow sensor 14 is recorded in memory within the ECU 40.

Thus, even while the exhaust flow rate control is performed and at the same time the EGR gas is introduced into the intake system, failure of the air flow sensor 14 can be detected with high accuracy, as in the first to third embodiments described above, whereby the reliability of the air flow sensor 14 can be improved.

FIG. 6 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed in the failure detection apparatus according to the fifth embodiment of the present invention. In the following description of the flowchart, only the differences between the fourth and fifth embodiments will be explained.

In the fifth embodiment, after the target throttle valve opening and the target EGR valve opening are set in Step S12', the fresh air quantity reference value is set immediately thereafter based on the target throttle valve

opening and the target EGR valve opening, in Step S16', without correcting the target openings, unlike the fourth embodiment.

Then, in Step S17, it is determined whether or not the
5 actual excess air ratio λ detected by the λ sensor 26 is equal to the target value λ_1 ($\lambda = \lambda_1$). If the decision in this step is affirmative (Yes) and it is judged that the actual excess air ratio λ and the target value λ_1 are equal to each other, it can be concluded that the target throttle
10 valve opening and the target EGR valve opening have been set to proper values matching their actual openings, and accordingly, the routine proceeds to Step S22.

On the other hand, if the decision in Step S17 is negative (No) and it is judged that the actual excess air
15 ratio λ and the target value λ_1 differ from each other, the overall opening of the intake and exhaust throttle valves 12 and 22 and the opening of the EGR valve 32 are corrected, in Step S18', such that the actual excess air ratio λ becomes equal to the target value λ_1 .

20 Namely, in the fourth embodiment, the target throttle valve opening and the target EGR valve opening are corrected so as to match their actual openings. In the fifth embodiment, the actual overall opening of the intake and exhaust throttle valves 12 and 22 and the actual
25 opening of the EGR valve 32 are corrected so as to match their target openings.

Thus, the actual overall opening of the intake and exhaust throttle valves 12 and 22 and the actual opening of the EGR valve 32 are corrected to proper values matching
30 their target openings, and accordingly, the fresh air quantity reference value can be set to a highly accurate value as in the case where the exhaust flow rate is not adjusted or the EGR gas is not introduced.

Consequently, failure of the air flow sensor 14 can be detected with precision, regardless of the exhaust flow rate adjustment or the EGR gas introduction, so that the reliability of the air flow sensor 14 can be improved.

5 FIG. 7 is a flowchart illustrating a control routine for air flow sensor (AFS) failure determination, executed in the failure detection apparatus according to the sixth embodiment of the present invention. In the following description of the flowchart, only the differences between
10 the sixth embodiment and the fourth or fifth embodiment will be explained.

In the sixth embodiment, after the target throttle valve opening and the target EGR valve opening are set in Step S12', the fresh air quantity reference value is set
15 immediately thereafter based on the target throttle valve opening and the target EGR valve opening in Step S16', like the fifth embodiment.

Then, in Step S17, it is determined whether or not the actual excess air ratio λ detected by the λ sensor 26 is
20 equal to the target value λ_1 ($\lambda = \lambda_1$). If the decision in this step is affirmative (Yes) and it is judged that the actual excess air ratio λ and the target value λ_1 are equal to each other, it can be concluded that the target throttle valve opening and the target EGR valve opening have been
25 set to proper values matching their actual openings, and accordingly, the routine proceeds to Step S22.

On the other hand, if the decision in Step S17 is negative (No) and it is judged that the actual excess air ratio λ and the target value λ_1 differ from each other, the
30 exhaust flow rate control and the EGR control are suspended in Step S19', then a normally obtained fresh air quantity Q_a is directly set as the fresh air quantity reference value in Step S20, and the routine proceeds to Step S22.

Namely, in the sixth embodiment, if there is a difference between the actual excess air ratio λ and the target value λ_1 , it is concluded that the fresh air quantity reference value cannot be set with accuracy, and
5 the exhaust flow rate control and the EGR control are suspended. Thus, using the fresh air quantity Q_a obtained normally in accordance with the operating state of the engine 1 as the fresh air quantity reference value, the air flow sensor 14 is diagnosed, without adjusting the exhaust
10 flow rate or introducing the EGR gas.

This permits the fresh air quantity reference value to be always set to an accurate value, without reducing the occasion for diagnosis and regardless of the degree to which the exhaust flow rate is adjusted or to which the EGR
15 gas is introduced. Also in this case, therefore, failure of the air flow sensor 14 can be detected with precision, making it possible to improve the reliability of the air flow sensor 14.

While the preferred embodiments of the present
20 invention have been described, it should be noted that the present invention is not limited to the foregoing embodiments alone.

For example, in the foregoing embodiments, the λ sensor (O_2 sensor etc.) 26 is used as the exhaust
25 concentration detecting means and the excess air ratio λ or air-fuel ratio of the exhaust system, which is detected by the λ sensor 26, is compared with the target value (predetermined value) λ_1 . The present invention is, however, not limited to such configuration and may be
30 provided with a means for detecting the concentration of gas flowing into the combustion chamber 2 so that the detected gas concentration may be compared with a predetermined value.

Also, in the foregoing embodiments, both the intake throttle valve 12 and the exhaust throttle valve 22 are provided as the exhaust flow rate adjusting means, but the exhaust flow rate adjusting means may be constituted by
5 either one of the intake and exhaust throttle valves 12 and 22.

Further, although in the foregoing embodiments, a diesel engine is used as the engine 1, the engine 1 may alternatively be a gasoline engine.